

February 10, 2023

# **STRUCTURAL SUPPORT CALCULATIONS** (Supplemental Calculations)

### **HEADRICK RESIDENCE**

8822 SE 62<sup>nd</sup> Street Mercer Island, WA 98040

Quantum Job Number: 21271.01

Prepared for: NED NELSON, ARCHITECT 1021 92<sup>nd</sup> Avenue NE Bellevue, Washington 98004

Prepared by: QUANTUM CONSULTING ENGINEERS 1511 Third Avenue, Suite 323 Seattle, WA 98101 TEL 206.957.3900 FAX 206.957.3901



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### **HEADRICK RESIDENCE**

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Quantum Job Number: 21271.01

# **DESIGN CRITERIA**

## Residential Building Loads

Roof

Snow Load

25 psf

Garage Roof Loads		Comments
Standard Roofing	4.0 psf	
3/4" Plywood Shtg	2.8 psf	
Trusses @ 24" o.c.	3.0 psf	
Insulation	1.0 psf	
Lights, ducts	0.5 psf	
5/8" GWB	2.8 psf	
Miscellaneous	0.9 psf	
Total:	15.0 psf	SL=25 PSF
		-

# Deflection Criteria

<u>Roof</u> Live Load: L/240 Total Load: L/240	<u>Walls</u>	L/120 L/240 L/240	*flexible finishes *brittle finish *supporting glass	<u>Floor</u> Live Load: <b>L/360</b> Total Load: <b>L/240</b>			
Quantum Consulting Engineer	s LLC	Projec	t: Headrick Residence	Date:	2/10/23	Job No:	21271.01
1511 Third Avenue, Suite 323				Designer:	MKS	Sheet:	1
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### **HEADRICK RESIDENCE**

8822 SE 62<sup>nd</sup> Street Mercer Island, WA 98040

Quantum Job Number: 21271.01

# **GRAVITY DESIGN**



21271.01 - Headrick Residence

Garage Roof			
Member Name	Results	Current Solution	Comments
West Wall Header, 10'-0"	Passed	1 piece(s) 5 1/8" x 9" 24F-V4 DF Glulam	
West Wall Header with Girder Truss, 10'-0"	Passed	1 piece(s) 5 1/8" x 9" 24F-V4 DF Glulam	
Garage Main Floor			
Member Name	Results	Current Solution	Comments
Garage Stud	Passed	1 piece(s) 2 x 6 HF No.2 @ 16" OC	

ForteWEB Software Operator
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Job Notes



2/10/2023 7:41:41 PM UTC ForteWEB v3.5 File Name: 21271.01 - Headrick Residence



### MEMBER REPORT



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	2684 @ 1 1/2"	9994 (3.00")	Passed (27%)		1.0 D + 1.0 S (All Spans)
Shear (lbs)	2173 @ 1'	9371	Passed (23%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-Ibs)	6714 @ 5' 3"	15913	Passed (42%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.122 @ 5' 3"	0.342	Passed (L/999+)		1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.227 @ 5' 3"	0.512	Passed (L/543)		1.0 D + 1.0 S (All Spans)

System : Wall Member Type : Header Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

• Deflection criteria: LL (L/360) and TL (L/240).

• Allowed moment does not reflect the adjustment for the beam stability factor.

• Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length L = 10' 3".

• The effects of positive or negative camber have not been accounted for when calculating deflection.

• The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.

Applicable calculations are based on NDS.

	Bearing Length		Loads to Supports (lbs)				
Supports	Total	Available	Required	Dead	Snow	Factored	Accessories
1 - Trimmer - HF	3.00"	3.00"	1.50"	1240	1444	2684	None
2 - Trimmer - HF	3.00"	3.00"	1.50"	1240	1444	2684	None

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	10' 6" o/c	
Bottom Edge (Lu)	10' 6" o/c	

•Maximum allowable bracing intervals based on applied load.

			Dead	Snow	
Vertical Loads	Location	Tributary Width	(0.90)	(1.15)	Comments
0 - Self Weight (PLF)	0 to 10' 6"	N/A	11.2		
1 - Uniform (PSF)	0 to 10' 6"	11'	15.0	25.0	Roof
2 - Uniform (PLF)	0 to 10' 6"	N/A	60.0	-	Wall Above

### Weyerhaeuser Notes

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator Job N Maxwell Skotheim Quantum Consulting Engineers (206) 957-3906 MSkotheim@quantumce.com

Job Notes





### MEMBER REPORT





All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	2833 @ 1 1/2"	9994 (3.00")	Passed (28%)		1.0 D + 1.0 S (All Spans)
Shear (lbs)	2762 @ 1'	9371	Passed (29%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-Ibs)	5170 @ 2'	15913	Passed (32%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.080 @ 4' 7 3/8"	0.342	Passed (L/999+)		1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.142 @ 4' 9 1/16"	0.512	Passed (L/863)		1.0 D + 1.0 S (All Spans)

System : Wall Member Type : Header Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

• Deflection criteria: LL (L/360) and TL (L/240).

• Allowed moment does not reflect the adjustment for the beam stability factor.

• Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length L = 10' 3".

• The effects of positive or negative camber have not been accounted for when calculating deflection.

• The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.

Applicable calculations are based on NDS.

	Bearing Length			Loads to Supports (lbs)			
Supports	Total	Available	Required	Dead	Snow	Factored	Accessories
1 - Trimmer - HF	3.00"	3.00"	1.50"	1068	1765	2833	None
2 - Trimmer - HF	3.00"	3.00"	1.50"	529	395	924	None

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	10' 6" o/c	
Bottom Edge (Lu)	10' 6" o/c	

•Maximum allowable bracing intervals based on applied load.

			Dead	Snow	
Vertical Loads	Location	Tributary Width	(0.90)	(1.15)	Comments
0 - Self Weight (PLF)	0 to 10' 6"	N/A	11.2		
1 - Uniform (PLF)	0 to 10' 6"	N/A	60.0	-	Wall Above
2 - Point (lb)	2'	N/A	850	2160	Girder Truss

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ForteWEB Software Operator	Job Notes
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MEMBER REPORT

### Garage Main Floor, Garage Stud 1 piece(s) 2 x 6 HF No.2 @ 16" OC

### Wall Height: 13'

Member Height: 12' 7 1/2"

O. C. Spacing: 16.00"

PASSED



Design Results	Actual	Allowed	Result	LDF	Load: Combination
Slenderness	28	50	Passed (55%)		
Compression (lbs)	1000	3832	Passed (26%)	1.00	1.0 D + 1.0 L
Plate Bearing (lbs)	1000	4177	Passed (24%)		1.0 D + 1.0 L
Lateral Reaction (lbs)	88			1.60	1.0 D + 0.6 W
Lateral Shear (lbs)	81	1320	Passed (6%)	1.60	1.0 D + 0.6 W
Lateral Moment (ft-lbs)	276 @ mid-span	1264	Passed (22%)	1.60	1.0 D + 0.6 W
Total Deflection (in)	0.22 @ mid-span	1.26	Passed (L/704)		1.0 D + 0.6 W
Bending/Compression	0.31	1	Passed (31%)	1.60	1.0 D + 0.45 W + 0.75 L + 0.75 Lr

Lateral deflection criteria: Wind (L/120)

• Input axial load eccentricity for this design is 16.67% of applicable member side dimension.

Applicable calculations are based on NDS.

• A bearing area factor of 1.25 has been applied to base plate bearing capacity.

• A 15% increase in the moment capacity has been added to account for repetitive member usage.

Supports	Туре		Material	System : Wall		
Тор	Dbl 2X		Hem Fir	Member Type : Stud		
Base	Base 2X		Hem Fir	Design Methodology : ASD		
				9		
Max Unbraced Length			Comments			

Drawing is Conceptual

Lateral Connections										
Supports	Connector	Type/Model	Quantity	Connector Nailing						
Тор	Nails	8d (0.113" x 2 1/2") (Toe)	2	N/A						
Base	Nails	8d (0.113" x 2 1/2") (Toe)	2	N/A						

Nailed connection at the top of the member is assumed to be nailed through the bottom 2x plate prior to placement of the top 2x of the double top plate assembly.

		Dead	Floor Live	
Vertical Load	Spacing	(0.90)	(1.00)	Comments
1 - Point (PLF)	16.00"	150.0	600.0	Roof

			Wind	
Lateral Load	Location	Spacing	(1.60)	Comments
1 - Uniform (PSF)	Full Length	16.00"	17.3	

ASCE/SEI 7 Sec. 30.4: Exposure Category (B), Mean Roof Height (33'), Topographic Factor (1.0), Wind Directionality Factor (0.85), Basic Wind Speed (98), Risk Category(II), Effective Wind Area

determined using full member span and trib. width. • IBC Table 1604.3, footnote f: Deflection checks are performed using 42% of this lateral wind load.

1

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

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### **HEADRICK RESIDENCE**

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Quantum Job Number: 21271.01

# LATERAL DESIGN





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project date project no. designer sheet client checked by

Structure: Headrick Garage Floor Level: Roof (N-S)

Depth of Floor Framing & Plates (Clearspan) at Interstory (in) =

1.17 12.00

Sds =

Shear Wall Line Information

SW Mark		L <sub>sw</sub> (ft)	Wall Pier h <sub>wp</sub> (ft)	Aspect Ratio	Wall Framing Species	Specific Gravity G	Interstory or Base?	h <sub>sw</sub> (ft)	Wall Wt. (psf)	Roof/Floor Trib. (ft)	Roof/Floor Wt. (psf)
SW GRID	1	36.00	-	-	-	-	-	-	-	-	-
SW Segment	1.1	36.00	13.00	0.36	HF #2	0.43	Base	13.00	10.0	11.0	15.0
SW GRID	2	31.33		-	-	-	-	-	-	-	-
011 012	2.1	31.33	13.00	0.41	HF #2	0.43	Base	13.00	10.0	11.0	15.0
SW GRID		0.00	· ·	-	-	-	-	-	-	-	-
SW GRID		0.00	•	-		-	-	-	-		

### Shear Wall Loads and Summary

SW Mark		EQ (Ib) Wall (ULT)	Wind (lb) Wall (ULT)	Wall DL (lb)	Wall DL (lb) End 1	Wall DL (lb) End 2	Shear Wall Type	MIN. # of End Studs	Holdown
SW GRID	1	1420	1220	-	-	-	-	-	-
SW Segment	1.10	1420	1220	10620	280	280	SW-6	2	No HD
SW GRID	2	1420	1220				-	-	-
	2.10	1420	1220	9243	280	280	SW-6	2	No HD
SW GRID							-	-	-
SW GRID							-	-	-



Quantum Consulting Engineers LLC	Project: Headrick Garage	Date:	2/10/23	Job No:	21271.01
1511 Third Avenue, Suite 323		Designer:	MKS	Sheet:	1
Seattle, WA 98101	Client: Ned Nelson	Checked By:			

Structure: Headrick Garage Floor Level: Roof (N-S)

Shear Wall Schedule (LF	Shear Wall Schedule (LRFD) \$									
Shear Wall Type	Sheathing Grade, Sheathing Thickness, & Nail Size	Panel Edge Nail Spacing (in)	Nominal Seismic SW Capacity (plf)	LRFD Seismic SW Capacity (plf)	Nominal Wind SW Capacity (plf)	LRFD Wind SW Capacity (plf)	Sheathing Shear Stiffness, G <sub>a</sub> (Ib/in)			
SW-6	APA Rated, 7/16", 8d Common	6	520	416	730	584	10			
SW-4	APA Rated, 7/16", 8d Common	4	760	608	1065	852	13			
SW-3	APA Rated, 7/16", 8d Common	3	980	784	1370	1096	15			
SW-2	APA Rated, 7/16", 8d Common	2	1280	1024	1790	1432	20			
2SW-4	APA Rated, 7/16", 8d Common	4	1520	1216	2130	1704	26			
2SW-3	APA Rated, 7/16", 8d Common	3	1960	1568	2740	2192	30			
2SW-2	APA Rated, 7/16", 8d Common	2	2560	2048	3580	2864	40			

\*\*See SDPWS Table 4.3A Note 2 Determine Shear Wall Type (LRFD)

SW Segment Mark	Seismic Shear (plf)	Aspect Ratio Reduction	Adjusted Seismic Shear (plf)	Wind Shear (plf)	Adjusted Wind Shear (plf)	Controlling Shear (plf)	Shear Wall Type	Shear Wall Capacity (plf)	Check	Controlling Shear
1.10	39	1.00	42	34	36	42	SW-6	416	ок	Seismic
2.10	45	1.00	49	39	42	49	SW-6	416	ОК	Seismic

Determine	Chase	M-11	<b>O</b>	M		
Determine	Snear	waii	Overturning	woment	Lever	AIII

<u>\*NOTE:</u> CONTROLLING SHEAR IS BASED ON THE DIFFERENCE IN SHEAR WALL CAPACITY BETWEEN WIND & EQ

Determine Onear Wan O	verturning wor	Interest Ann			
SW Segment Mark	Wall Length Lever Arm (ft)	Calculated Lever Arm (ft)	% Different	Override Wall Length	User Input M <sub>OT</sub> Lever Arm (ft)
1.10	36.00	35.63	1.05%	No	
2 10	31 33	30.96	1 21%	No	
2.10	01.00	30.30	1.21/0		
	<u> </u>				
	1				
	+				
	+				

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Seattle, WA 98101	Client: Ned Nelson	Checked By:			

Structure: Headrick Garage Floor Level: Roof (N-S)

### Shear Wall End Axial Load (ASD)

SW Segment Mark	Seismic Tension (Ib)	ASD Seismic Tension Above (Ib)	Seismic Tension Total (Ib)	Wind Tension (lb)	ASD Wind Tension Above (Ib)	Wind Tension Total (Ib)	End 1 Dead (Ib)	End 2 Dead (Ib)
1.10	359		359	264		264	5590	5590
2.10	412		412	304		304	4902	4902

### Determine Required Holdown (ASD)

SW Segment Mark	Wind End 1 Eq. 16-15	EQ End 1 Eq. 16-16	Wind End 2 Eq. 16-15	EQ End 2 Eq. 16-16	Controlling Ten. Load (lb)	Holdown	Holdown Capacity (Ib)	Status
1.10	3090	2079	3090	2079	2079	No HD	0	ок
2.10	2637	1726	2637	1726	1726	No HD	0	ОК
	1				1			



Structure: Headrick Garage Floor Level: Roof (E-W)

Depth of Floor Framing & Plates (Clearspan) at Interstory (in) =

1.17 12.00

Sds =

Shear Wall Line Information

SW Mark		L <sub>sw</sub> (ft)	Wall Pier h <sub>wp</sub> (ft)	Aspect Ratio	Wall Framing Species	Specific Gravity G	Interstory or Base?	h <sub>sw</sub> (ft)	Wall Wt. (psf)	Roof/Floor Trib. (ft)	Roof/Floor Wt. (psf)
SW GRID	Α	18.00	-	-	-	-	-	-	-	-	-
SW Segment	A.1	18.00	13.00	0.72	HF #2	0.43	Base	13.00	10.0	2.0	15.0
SW GRID	В	4.00	-	-	-	-	-	-	-	-	-
	B.1	2.00	4.00	2.00	HF #2	0.43	Base	4.00	10.0	2.0	15.0
	B.2	2.00	4.00	2.00	HF #2	0.43	Base	4.00	10.0	2.0	15.0
SW GRID		0.00	-	-	-	-	-	-	-	-	-
SW GRID		0.00	-	-	-	-	-	-	-	-	-
					1					1	

### Shear Wall Loads and Summary

SW Mark		EQ (Ib) Wall (ULT)	Wind (lb) Wall (ULT)	Wall DL (lb)	Wall DL (lb) End 1	Wall DL (lb) End 2	Shear Wall Type	MIN. # of End Studs	Holdown
SW GRID	Α	1420	2150	-	-	-	-	-	-
SW Segment	A.1	1420	2150	2880	560	560	SW-6	2	No HD
SW GRID	В	1420	2150				-	-	-
	B.1	710	1075	140	560	560	SW-6	2	HDU2 (3075DF,2215HF)
	B.2	710	1075	140	560	560	SW-6	2	HDU2 (3075DF,2215HF)
SW GRID							-	-	-
SW GRID							-	-	-



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Structure: Headrick Garage Floor Level: Roof (E-W)

Shear Wall Schedule (LF	Shear Wall Schedule (LRFD) 👳								
Shear Wall Type	Sheathing Grade, Sheathing Thickness, & Nail Size	Panel Edge Nail Spacing (in)	Nominal Seismic SW Capacity (plf)	LRFD Seismic SW Capacity (plf)	Nominal Wind SW Capacity (plf)	LRFD Wind SW Capacity (plf)	Sheathing Shear Stiffness, G <sub>a</sub> (Ib/in)		
SW-6	APA Rated, 7/16", 8d Common	6	520	416	730	584	10		
SW-4	APA Rated, 7/16", 8d Common	4	760	608	1065	852	13		
SW-3	APA Rated, 7/16", 8d Common	3	980	784	1370	1096	15		
SW-2	APA Rated, 7/16", 8d Common	2	1280	1024	1790	1432	20		
2SW-4	APA Rated, 7/16", 8d Common	4	1520	1216	2130	1704	26		
2SW-3	APA Rated, 7/16", 8d Common	3	1960	1568	2740	2192	30		
2SW-2	APA Rated, 7/16", 8d Common	2	2560	2048	3580	2864	40		

\*\*See SDPWS Table 4.3A Note 2 Determine Shear Wall Type (LRFD)

SW Segment Mark	Seismic Shear (plf)	Aspect Ratio Reduction	Adjusted Seismic Shear (plf)	Wind Shear (plf)	Adjusted Wind Shear (plf)	Controlling Shear (plf)	Shear Wall Type	Shear Wall Capacity (plf)	Check	Controlling Shear
A.1	79	1.00	85	119	128	128	SW-6	584	ОК	Wind
B.1	355	1.00	382	538	578	578	SW-6	584	ок	Wind
B.2	355	1.00	382	538	578	578	SW-6	584	ОК	Wind

Determine Shear Wall Overturning Memont Lever Ar	
Determine Shear wan Overturning woment Lever Ar	n

<u>\*NOTE:</u> CONTROLLING SHEAR IS BASED ON THE DIFFERENCE IN SHEAR WALL CAPACITY BETWEEN WIND & EQ

SW Segment Mark	Wall Length Lever Arm (ft)	Calculated Lever Arm (ft)	% Different	Override Wall Length	User Input M <sub>OT</sub> Lever Arm (ft)
A.1	18.00	17.63	2.13%	No	
B.1 B.2	2.00 2.00	1.52 1.52	31.96% 31.96%	No No	

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Seattle, WA 98101	Client: Ned Nelson	Checked By:			

Structure: Headrick Garage Floor Level: Roof (E-W)

### Shear Wall End Axial Load (ASD)

SW Segment Mark	Seismic Tension (Ib)	ASD Seismic Tension Above (Ib)	Seismic Tension Total (Ib)	Wind Tension (lb)	ASD Wind Tension Above (Ib)	Wind Tension Total (Ib)	End 1 Dead (Ib)	End 2 Dead (Ib)
A.1	718		718	932		932	2000	2000
B 1	004		004	1200		1200	630	630
B.2	994		994	1290		1290	630	630

### Determine Required Holdown (ASD)

SW Segment Mark	Wind End 1 Eq. 16-15	EQ End 1 Eq. 16-16	Wind End 2 Eq. 16-15	EQ End 2 Eq. 16-16	Controlling Ten. Load (lb)	Holdown	Holdown Capacity (Ib)	Status
A.1	268	155	268	155	155	No HD	0	ок
B.1	-912	-719	-912	-719	-912	HDU2 (3075DF,2215HF)	-2215	ок
B.2	-912	-719	-912	-719	-912	HDU2 (3075DF,2215HF)	-2215	ОК
						<u>∧</u>		
						1	1	

Substitute Simpson STHD10 at –Shear Walls B.1 and B.2, Holdown Capacity = 1960lb, OK

Quantum Consulting Engineers LLC	Project: Headrick Garage	Date:	2/10/23	Job No:	21271.01
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